

1 A METHOD OF STIMULATING BLOOD-DERIVED COMPONENTS

2 USING NO ADDED THROMBIN OR OTHER AGONIST

by

4 Dr. Calvin Britton and Calvin Britton

5 Cross References

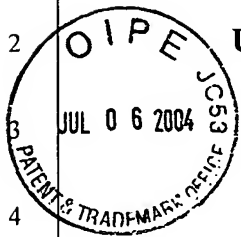
6 None.

7 Government Rights

8 None.

9 Background of the Disclosure

10 In the field wound care, it is a known strategy to separate whole blood
11 into various sub-components and to apply stimulated sub-components to
12 damaged tissue in an effort to accelerate, augment, or effectuate the tissue
13 repair, closure, and healing process. It is generally understood that the whole
14 blood is separated by centrifugation, sequestration, filtration, or other
15 mechanical process such that at least three dominant components are isolated
16 based on molecular weight or size. At least three components are understood
17 to result from such traditional separation, including but not limited to red
18 blood cells, platelet-poor plasma, and platelet-rich plasma. The platelet-rich
19 plasma may comprise platelets, white blood cells, fibrinogen, plasma, stem
20 cells and plasma proteins.



1 Generally, in connection with creating a tissue sealant and/or filler for use
2 in acute or chronic wound healing and damaged tissue repair, the prior art
3 attempts to activate the platelet rich plasma or the platelet-poor plasma
4 portions by saturating either the platelet rich or platelet poor plasma portion
5 with significant amounts of bovine-derived thrombin, collagen, serotonin, or
6 other agonist. Following such activation, it is known that a variety of cellular
7 pathways are triggered in such a way as to inevitably increase the viscosity of
8 the plasma portion(s). For example, it is understood that, as part of these
9 pathways and following the introduction of an agonist, fibrinogen present in
10 the plasma portion will transform into fibrin. There is substantial evidence in
11 the prior art that bovine-derived thrombin is applied in copious amounts in
12 order to activate the respective plasma portions and/or platelet concentrates.
13 For example, U.S. Patent No. 6,524,568 indicates a range between 100 U and
14 10,000 U exogenous thrombin as mixed with an 8mL platelet concentrate
15 volume, and the patent claims a preferred amount of 1000 U thrombin per 8 ml
16 of platelet concentrate.

17 The use of bovine or non-human-derived products is a widely used
18 phenomenon. All this may be in accepted practice today, yet the inventor
19 understands that it is best to significantly depart from the use of bovine-
20 derived products in connection with the unsafe circumstances surrounding

1 bovine spongiform encephalitis, known as BSE. As such, because it is very
2 difficult at this point in time to even test for infection of BSE, the inventor
3 invested substantial time and effort into formulating a method and procedure
4 whereby no exogenously-applied thrombin or similar agonist is utilized.
5 Obviously, because thrombin is endogenous to mammals, the inventor makes
6 clear that this patent does not seek to neutralize or vitiate endogenous
7 thrombin.

8 Thus, while exogenous thrombin is the current protocol in activating
9 either platelet-rich plasma or platelet-poor plasma, the disclosure herein serves
10 to satisfy in part, the goal of eliminating the reliance on super-saturation levels
11 of exogenously applied thrombin, be the source of such thrombin derived from
12 bovine sources or the product of concentration of the patient's own thrombin.
13 It is believed that the reduction in exogenously-applied thrombin will translate
14 into elevated confidence in certain medical procedures, easier compliance with
15 federal regulations governing exogenously applied chemicals in the health care
16 industry, and decreased cost in obviating the need for high-cost purification of
17 bovine-derived thrombin or similar agonist.

18 Summary

19 This disclosure relates to the stimulation of blood plasma portions by
20 creating a steady rate turgid gas and plasma portion interface. By creating a

1 turgid gas/liquid interface, under controlled conditions, this disclosure thus
2 seeks to activate the biological components associated with tissue repair and
3 wound care in a manner that reduces exogenous chemical contact or
4 treatments. In application, the inventor contemplates stimulating platelet rich
5 plasma by careful percolation or injection of oxygen gas through an amount of
6 platelet-rich plasma, although the same principles apply in either platelet-poor
7 plasma or with whole blood as well.

8 In the first preferred embodiment discussed below, no exogenous
9 thrombin was required to stimulate a sample of platelet rich plasma and
10 corresponding platelets and other factors present within the platelet rich
11 plasma.

12 It is therefore an object of the present disclosure to provide a combination
13 comprising a therapeutic amount of autologous platelet-rich plasma that
14 utilizes no exogenous thrombin yet nonetheless facilitates tissue sealing, repair,
15 healing, and wound closure.

16 It is still further object of the present disclosure to provide an efficient
17 method to stimulate platelet rich plasma by using steady gas percolation as
18 means to create an active turgid gas/liquid interface, which obviously differs
19 from the resting state gas/liquid interface occurring when the platelet rich
20 plasma is simply exposed to ambient air in an open container.

1 It is still further object of the present disclosure to provide a preparation of
2 concentrated platelet-rich plasma using an apparatus that permits ease of
3 application of stimulated platelet-rich plasma to damaged tissue.

4 It is still further object of the present disclosure to provide a preparation of
5 autologous platelet-rich plasma in a clinical environment to permit patients
6 who experience acute, chronic, or recurrent wound procedures. Such
7 benefiting procedures would include, but not be limited to, diabetic ulcers,
8 venous, decubitus, surgical dehiscences wounds, bone repair and tissue
9 remodeling in autologous wound care.

10 Towards the fulfillment of these and other objects and advantages, the
11 present method relates to a first step of isolating from the patient an amount of
12 whole blood and subjecting the whole blood to treatment with an anti-
13 coagulant agent, followed by a centrifugation or separation process to obtain an
14 amount of platelet-rich plasma. The second step comprises adding an effective
15 amount of anti-coagulant neutralizing reagent. The third step comprises
16 stimulating the platelet-rich plasma by creating a turgid gas/liquid interface.
17 The platelet rich plasma, once properly stimulated following the creation of the
18 turgid gas/liquid interface, will adopt certain characteristics such as increased
19 viscosity and fibrin formation. The fourth step comprises applying the
20 stimulated platelet rich plasma to, or infused within, damaged tissue.

Description

The first preferred embodiment discussed in more detail below represents a process wherein the first step comprises isolating from the patient whole blood using venipuncture. As part of this isolation, it is preferable to receive the whole blood in a container that is treated with an effective amount of anti-clotting agent such as sodium citrate. Using platelet pheresis equipment, blood sequestration or separation mechanisms, the whole blood is thereafter centrifuged or otherwise processed and thereby separated into generally distinct components; i.e., the platelet-rich plasma, the platelet-poor plasma, and the red blood cell concentrates.

To initiate the second step, the technician or apparatus isolates the platelet-rich plasma and combines an effective amount of neutralizing agent to counter the effects of the anticoagulating agent. Calcium chloride is an effective anti-coagulant neutralizing agent, although other agents may be used interchangeably.

The third step involves creation of a steady turgid gas/liquid interface by way of percolating through the platelet-rich plasma a steady stream of gas which in turn stimulates the platelet-rich plasma and triggers the transformation of fibrinogen to fibrin. Within a relatively brief period of time, the viscosity of the platelet-rich plasma will increase. Variability in stimulation

1 created by the turgid gas/liquid interface depends upon the volume of platelet-
2 rich plasma when compared to the size of the gas bubbles and the relative
3 speed and rate of percolation of gas through the platelet-rich plasma, although
4 there are generalized parameters, exemplified generally thorough the Examples
5 recited herein.

6 Following the stimulation of the platelet rich plasma, the platelet rich
7 plasma will become viscous and gelatin-like. Once the platelet rich plasma
8 becomes viscous, it is generally known as a tissue graft. As the fourth step, the
9 tissue graft may then be molded, sculpted, or crafted to fit within, applied to,
10 co-saturated with dried or donor material(s), induced into or applied around
11 various grafts, appliances, tools, apparatus, or other fixtures or dressings used
12 with bone or soft tissue repair, remodeling, sealing or healing a particular
13 wound or tissue injury site or to fill surgical incisions.

14 It is generally desirable for platelet rich plasma, once initially stimulated,
15 to transform into a tissue graft in not more than fifteen minutes. Using the
16 process described herein, the desired viscosity of the tissue graft was reliably,
17 and consistently, obtained in less than fifteen minutes. This time period is
18 acceptable for the industry. In fact, using exogenously-applied thrombin
19 concentrations otherwise referenced in U.S. Patent No. 6,524,568, the formation
20 of the viscous platelet graft occurred also within 15 minutes. Of course, the

1 variability associated with the time it takes for the platelet rich plasma to
2 become first stimulated and when the platelet-rich plasma changes viscosity
3 and form a tissue graft varies from patient to patient, and one cause for such
4 variability appears to be a function of the fibrinogen or platelet levels of the
5 patient. When using the steady percolation method, another source of
6 variability appears to be a function of the size of the gas bubbles and the rate,
7 platelet rich plasma ("PRP") volume, and speed of percolation.

8 In a second preferred embodiment, the goal is to simply remove from the
9 whole blood the majority of red blood cells. It is the inventor's experience that
10 the introduction of red blood cells into a wound exacerbates wound healing.

11 For that reason, the second preferred embodiment contemplates the use of that
12 portion of plasma, platelets, fibrinogen, white blood cells, and other cellular
13 structures, as long as the number of red blood cells is reduced when compared
14 to whole blood. Existing technology permits easy isolation of red blood cells,
15 so this disclosure does not contemplate any one mode of centrifugation,
16 sequestration, filtration or separation process over another; instead, this
17 disclosure contemplates a need to separate out red blood cells from the whole
18 blood to decrease the ill-effects associated with degradation of red blood cells
19 within such damaged tissue once the stimulated tissue graft is applied to the

1 damaged tissue. The activation process in the second preferred embodiment is
2 disclosed in the first preferred embodiment.

3 EXAMPLE 1

4 Whole blood was collected from the antecubital vein in the arm into a
5 container with an appropriate amount of anticoagulant agent, sodium citrate,
6 and processed by centrifugation to sequester platelet rich plasma. The platelet
7 rich plasma was combined with .05cc 10% CaCl per 1cc of platelet rich plasma
8 in order to neutralize the effects of the anticoagulant. The platelet rich plasma
9 was then gently and steadily bubbled (10 bubbles per second) with Oxygen gas
10 to stimulate the platelet rich plasma. The gas was percolated for fifteen
11 minutes or until the platelet rich plasma converted from a liquid form into a
12 substantially gelatinous form. This entire transformation generally takes less
13 than fifteen (15) minutes. The size of the bubble was an estimated 4 mm in
14 diameter.

15 EXAMPLE 2

16 Using the same procedure in Example 1 to isolate platelet rich plasma, and
17 thereafter treating the platelet rich plasma with anti-coagulant neutralizer, the
18 platelet rich plasma was gently and steadily bubbled (1 bubble per second)
19 with Oxygen gas to stimulate the platelet rich plasma. The gas was percolated
20 for up to fifteen (15) minutes, until the platelet rich plasma converted from a

1 liquid form into a substantially gelatinous form. The size of the bubble was an
2 estimated 4 mm in diameter.

3 EXAMPLE 3

4 Using the same procedure in Example 1 to isolate platelet rich plasma and
5 thereafter neutralize the anti-coagulant, the platelet rich plasma was steadily
6 bubbled using a rolling bubble stream (15-50 bubbles per second) with Oxygen
7 gas to stimulate the platelet rich plasma. The gas was initially percolated for
8 two (2) minutes using this rolling bubble stream and then removed, permitting
9 the platelet rich plasma to sit idle in order to facilitate opportunity for the blood
10 components to build the necessary latticework and structural cross-linking and
11 become more viscous. This entire transformation generally takes
12 approximately ten (10) minutes. The size of the bubble was an estimated 4 mm
13 in diameter, although bubbles as large as 1 cm have proven successful.

14 Under the three above examples, the tissue graft is uniform across all
15 surfaces and throughout.

16 EXAMPLE 4

17 Whole blood was collected from the antecubital vein in the arm into a
18 container with an appropriate amount of anticoagulant agent, sodium citrate,
19 and processed by centrifugation to sequester primarily platelet rich plasma.
20 The platelet rich plasma was combined with .05cc 10% CaCl per 1cc of platelet

1 rich plasma in order to neutralize the effects of the anticoagulant. The platelet
2 rich plasma was then gently and steadily bubbled (10 bubbles per second) with
3 Nitrogen gas to stimulate the platelet rich plasma. The gas was percolated for
4 three minutes or until the platelet rich plasma converted from a liquid form
5 into a substantially gelatinous form. This entire transformation generally takes
6 less than fifteen (15) minutes. The size of the bubble was an estimated 4 mm in
7 diameter.

8 EXAMPLE 5

9 Using the same procedure in Example 1 to isolate platelet rich plasma and
10 thereafter neutralize the anti-coagulant, the platelet rich plasma was thereafter
11 divided into two equal quantities and placed in two equal glass beakers, such
12 beakers being designated "first beaker" and the second designated "second
13 beaker." The first beaker was percolated with Oxygen gas at a rate of
14 approximately 5 bubbles per second for 13 minutes, and the platelet rich
15 plasma in the first beaker thereafter formed a viscous and expected graft
16 material. Over the same duration, the second beaker, exposed simply to
17 ambient air, showed no signs of stimulation, and there were no visible clots or
18 increased viscosity.

19 The foregoing examples do not necessarily limit the scope of the
20 disclosure herein, and it is only provided to establish actual step-by-step

1 methods by which the invention herein can be utilized effectively to achieve
2 platelet rich plasma gels without exogeneous application of thrombin or other
3 agonist.
4